



# ***Modeling Lubrication System Oil Flow***

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Mahle Metal Leve S.A.***

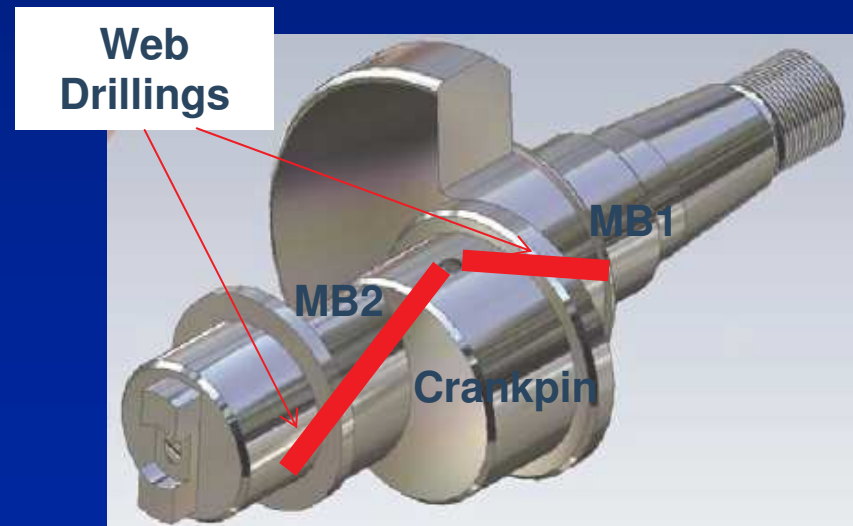
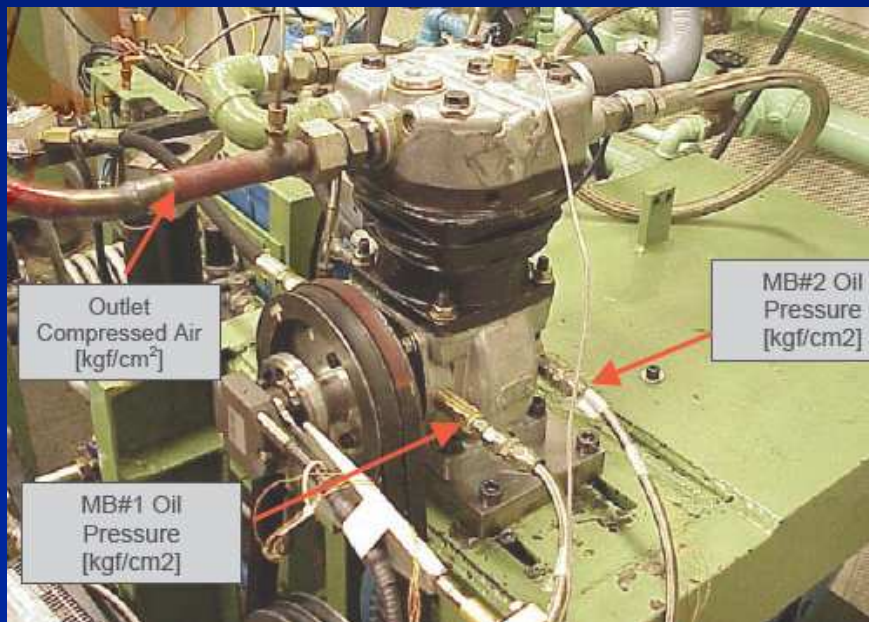
***Jon Harrison and Shawn Harnish, GTI***

## ***Gamma Technologies***

# 1-Cylinder Engine Lab Setup



- Motivation: to calculate flow distribution to each bearing (MB1, CR LEB, MB2) of a KNORR-BREMSE air compressor LK38
- 3 separate experiments (steps) performed
  - 1) baseline
  - 2) MB1 plugged
  - 3) MB2 plugged

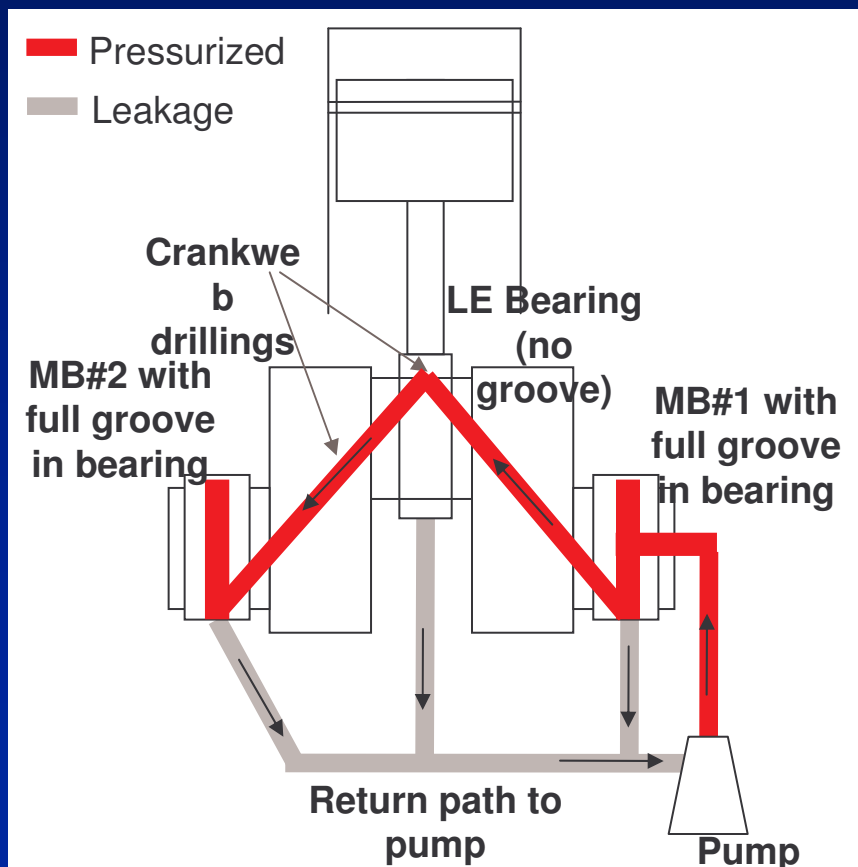


# Experimental Setup: Step 1



## • Step 1: Baseline Case

- Pump set to a particular flow rate (between 4–14 L/hr)
  - Inlet temp., MB1 and MB2 housing temp., and pressure in MB1 and MB2 measured



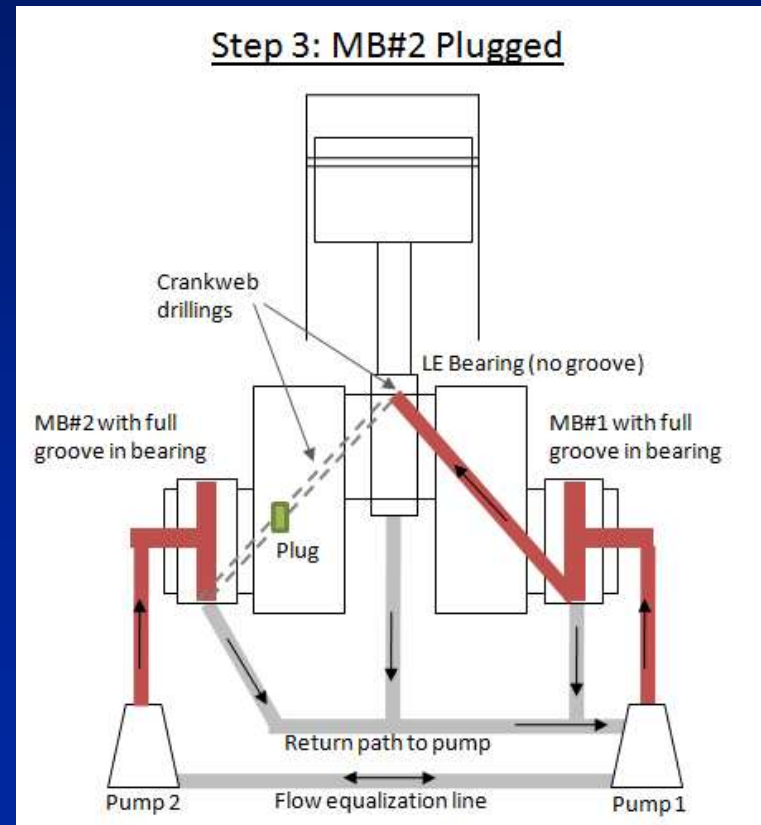
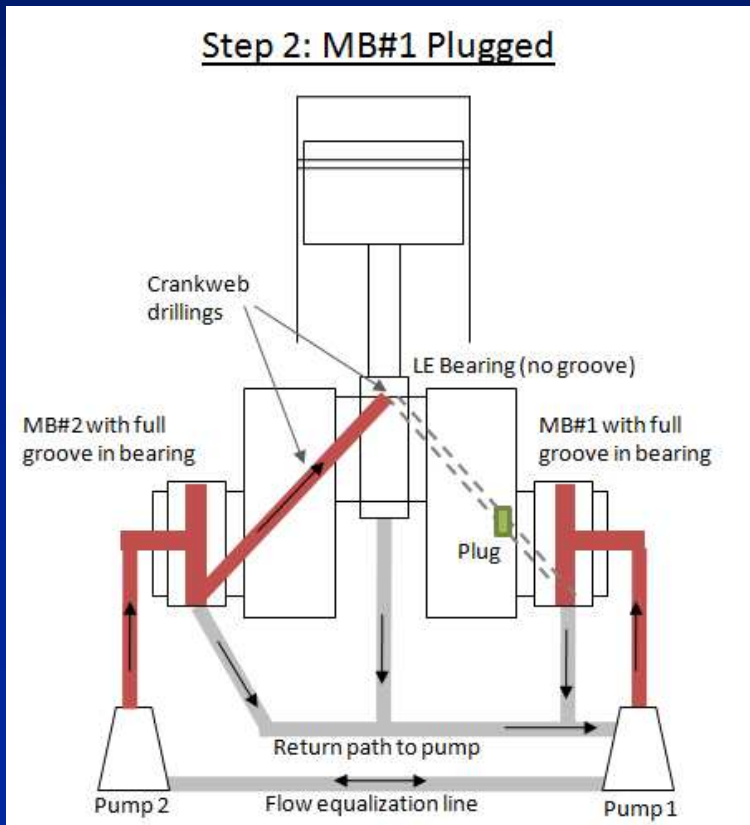
Oil 15W40  
Bore 88 mm  
Stroke 37 mm  
Peak Cylinder Pressure (Abs.) 8.8 bar

MB Dia 30 mm  
MB Bearing Width 16 mm  
MB1 Radial Clearance 0.0565 mm  
MB2 Radial Clearance 0.05 mm  
CR LEB Dia 42 mm  
CR LEB Radial Clearance 0.017 mm



## Experimental Setup: Steps 2 and 3

- Step 2 and 3:
  - Flow rate tuned in pump 1 and pump 2 to match pressure and temperature in each main bearing to baseline case (Step 1)
    - Isolating each main bearing allows the con rod large end bearing flow rate to be estimated

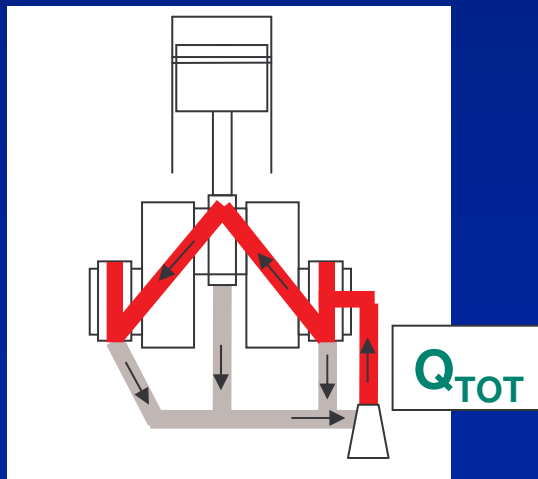


# Connecting Rod Large End Bearing Flow Rate Calculation

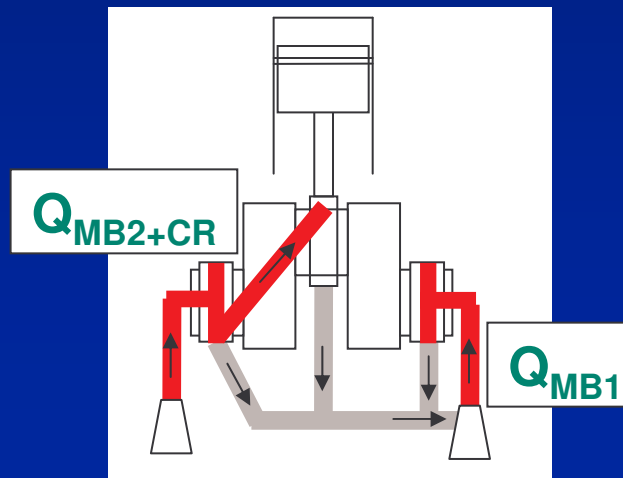


- Conrod Bearing Flowrate,  $Q_{CR}$ , calculated as average of three separate flow rate calculations:
  - $Q_{CR} = (Q_{CR1} + Q_{CR2} + Q_{CR3})/3$
  - $Q_{CR1} = Q_{TOT} - Q_{MB1,Step2} - Q_{MB2,Step3}$
  - $Q_{CR2} = Q_{MB2+CR,Step2} - Q_{MB2,Step3}$
  - $Q_{CR3} = Q_{MB1+CR,Step3} - Q_{MB1,Step2}$

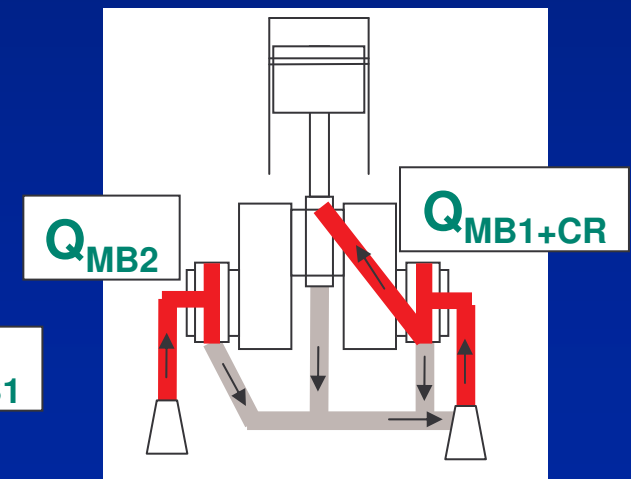
STEP 1



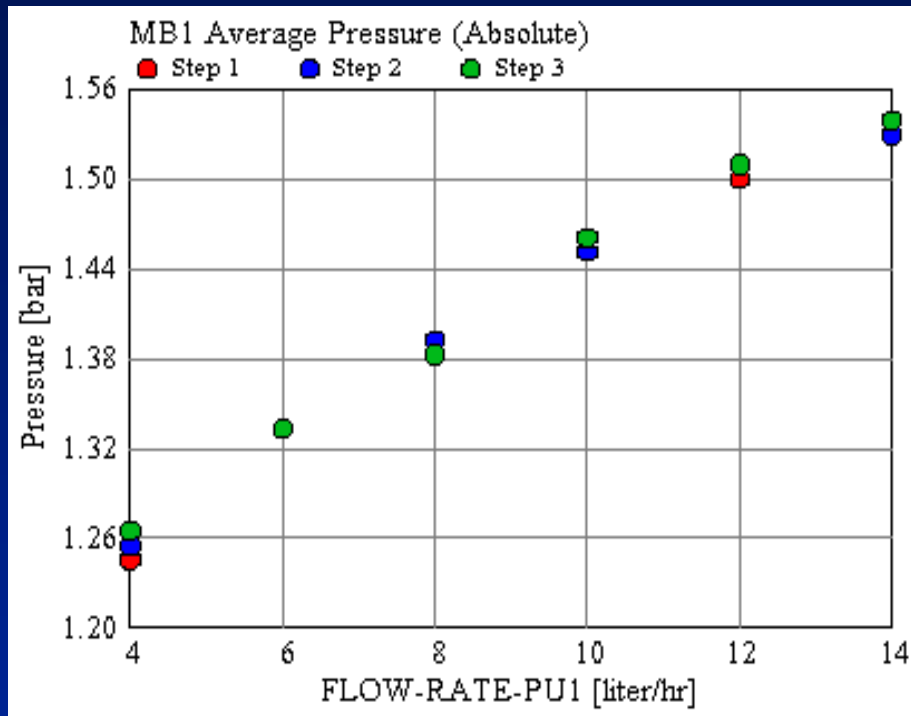
STEP 2



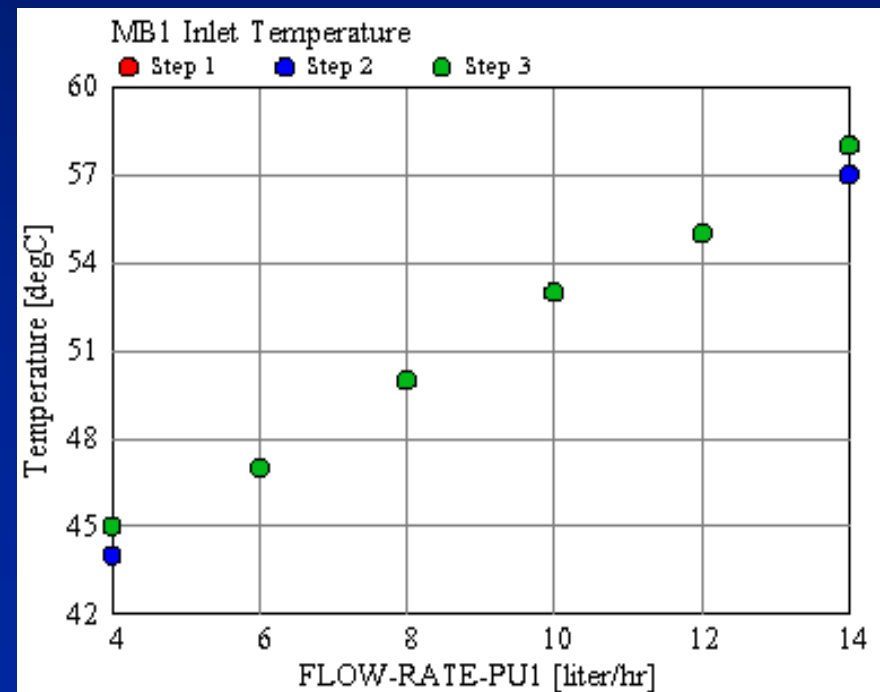
STEP 3



# Experimental Results: MB1



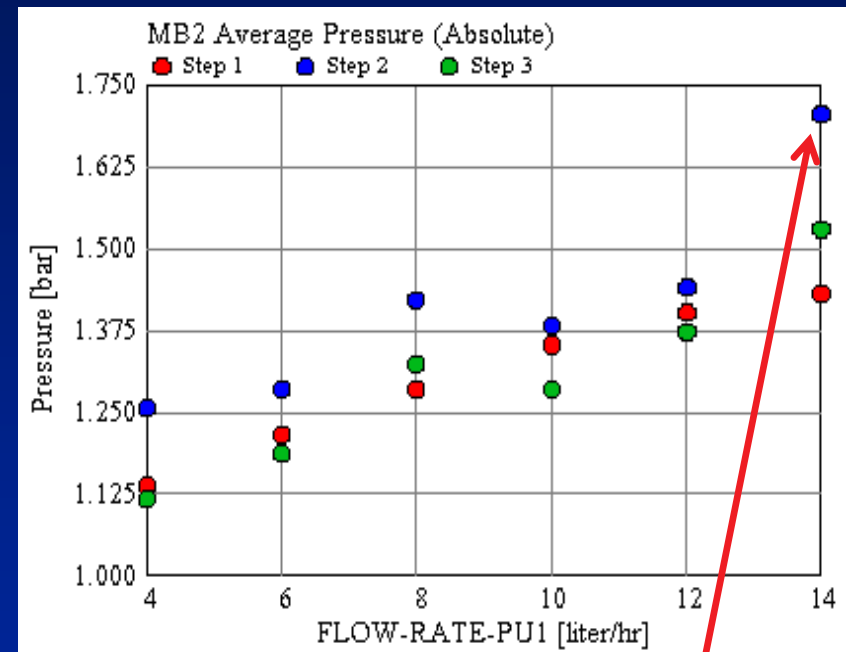
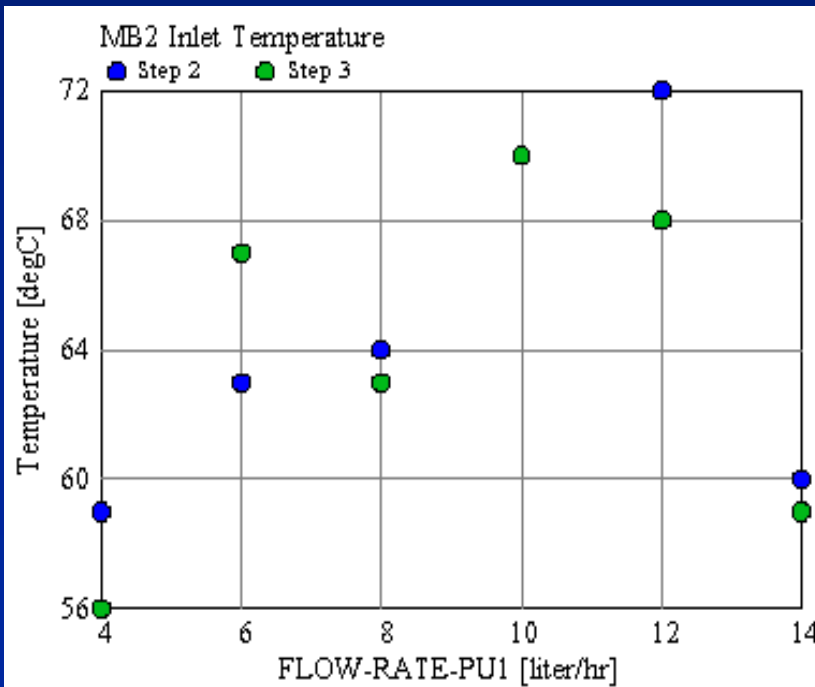
- MB#1 P and T consistent for all 3 steps



# Experimental Results: MB2



- MB#2 P and T inconsistent between steps
  - Reason: Pump#2 flow rate and heater hard to control

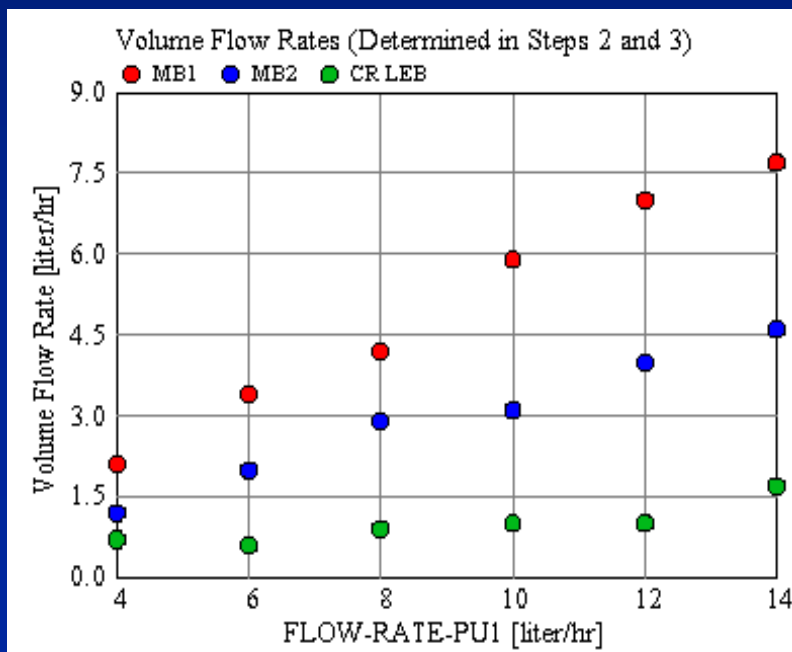
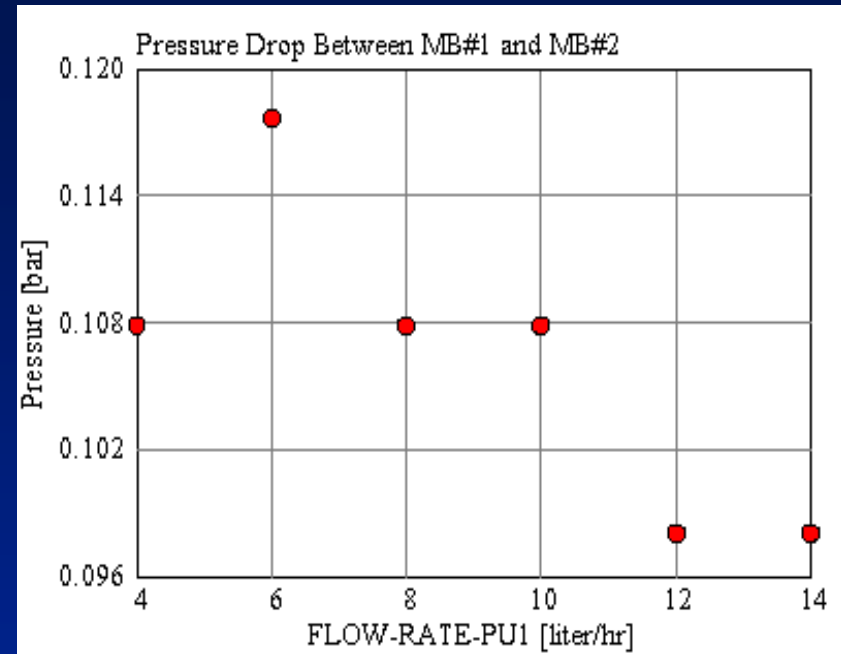


Pressure is high due to low inlet temperature (low temp = higher viscosity = higher pressure for a given flow rate)

# Experimental Results



- $\Delta P \sim \text{constant}$  vs. total pump flow rate for baseline case (Step 1)
  - Theory predicts  $\Delta P \sim Q^2$



- Flow rates determined in steps 2 and 3
- $Q_{\text{MB\#1}} > Q_{\text{MB\#2}}$ 
  - Reasons:
    - MB#1 clearance > MB#2 clearance
    - MB#1 pressure > MB#2 pressure

# General Model Setup: Step 1



Bearing loads automatically calculated from cylinder pressure and engine geometry/inertia

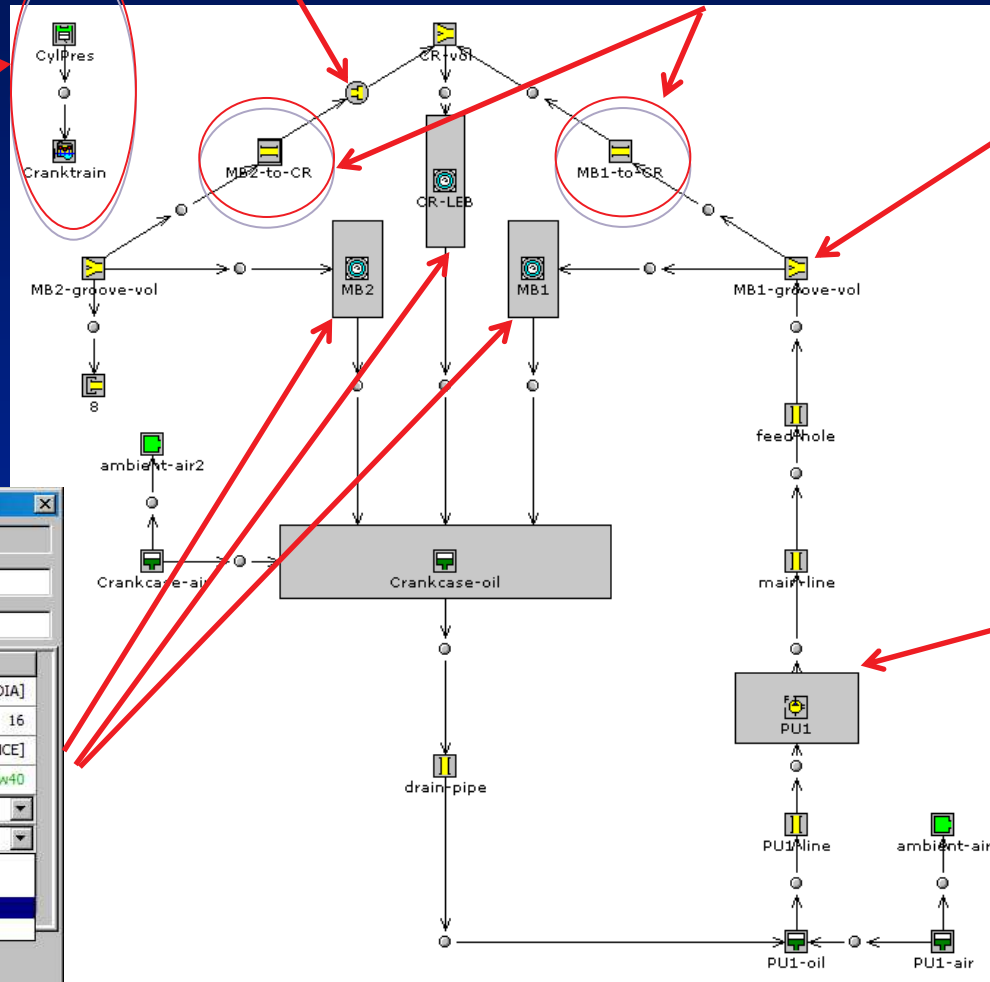
Bearing info defined in the BearingFlowEngine object

Attribute	Unit	Object Value
Bearing Diameter	mm	[MB2-DIA]
Bearing Width	mm	16
Bearing (radial) Clearance	mm	[MB2-CLEARANCE]
Oil Property Object		oil-15w40
Bearing Flow Model		Instantaneous
Instantaneous Flow Rate Solution		Feed Flow
Flow Rate Multiplier		Martin Eq.
Fraction of Conducted Friction Heat	fraction	Feed+Hydr. Flow
		Feed Flow
		[INSFLOPT]

Buttons: Main, Speed & Load, Groove/Hole, OK, Cancel

Orifice models restriction between web drillings

Web drillings account for centrifugal acceleration



Main bearing groove volume

Pump imposes flow rate

# Model Setup: Steps 2 and 3



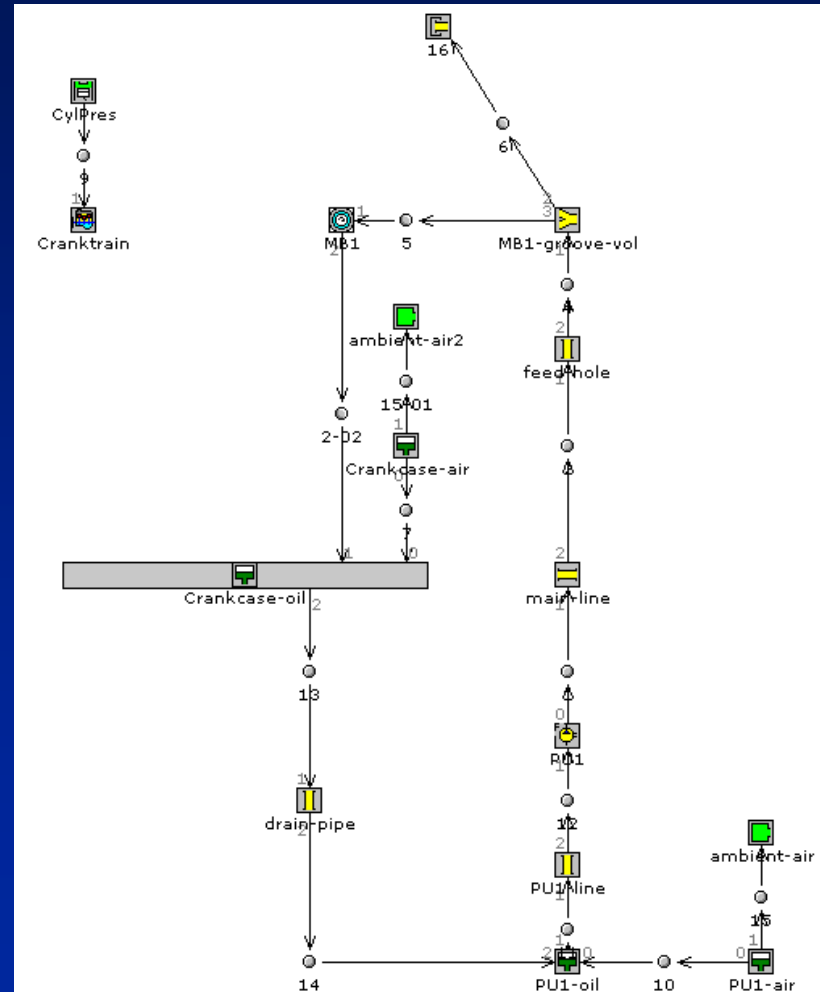
## Experiment:

- Flow rate was tuned to match pressure in MB1 of baseline case
- Temperature of fluid was tuned to match baseline case

## Model:

- Pump flow rate and temperature of MB1 are imposed based on experiment
  - Pressure in MB1 predicted

\* Same procedure done for MB2



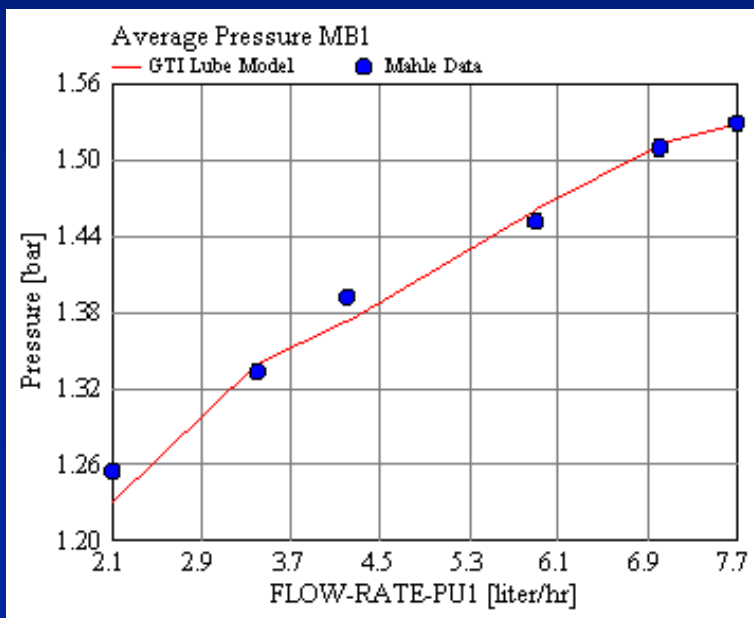


## Model Results: Steps 2 and 3

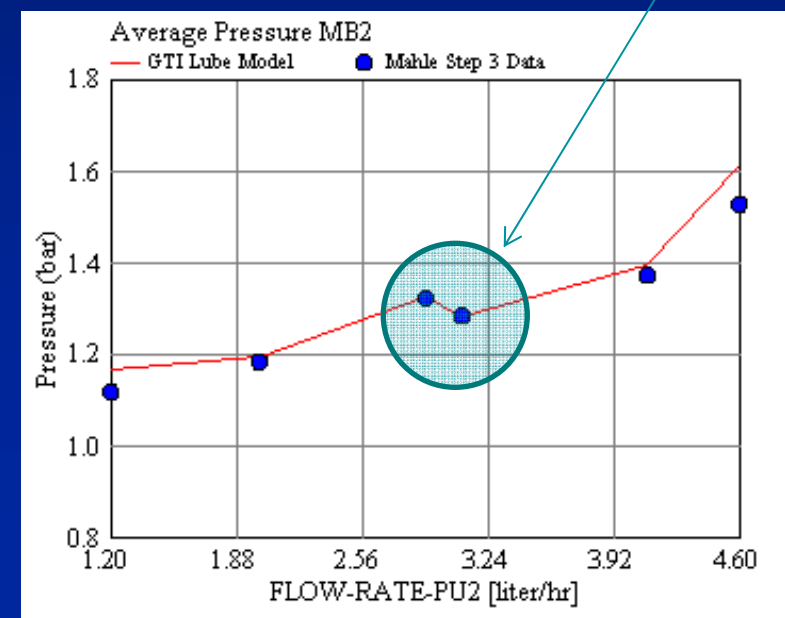
- Cycle averaged pressure in main bearings vs. flow rate provided by the pump
- Pressure in both bearings by themselves matches well to experimental data
- No tuning of the model required
  - bearing clearances within limits

Model captures experimental pressure drop due to temperature increase (see temp data from previous slide)

### MB1 Pressure



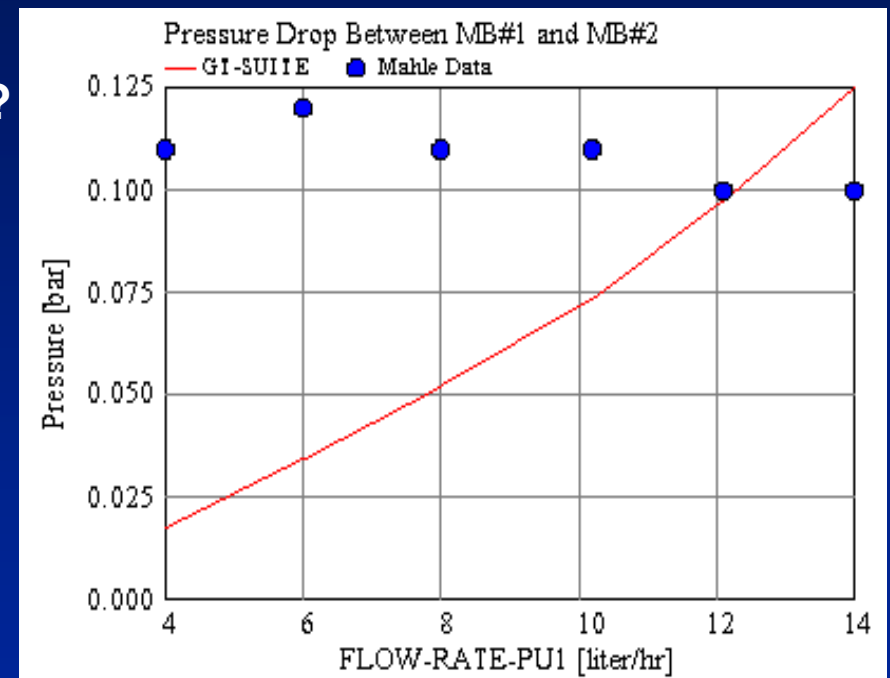
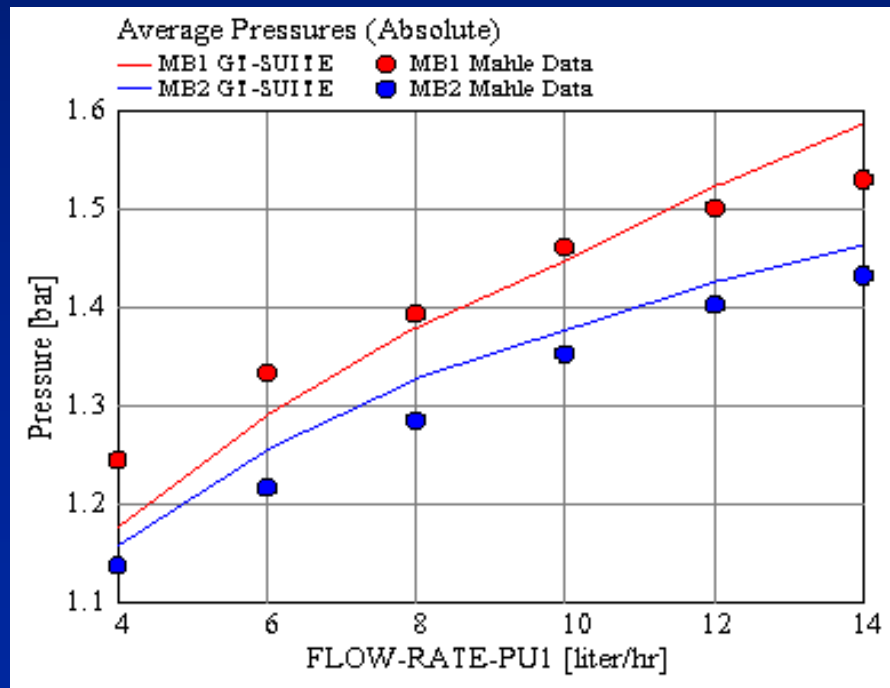
### MB2 Pressure





## Model Results: Step 1

- Model does not predict a constant  $\Delta P$  vs. Q relationship as seen in experiment
  - Is experimental data flawed?
  - Not modeling unknown phenomena?

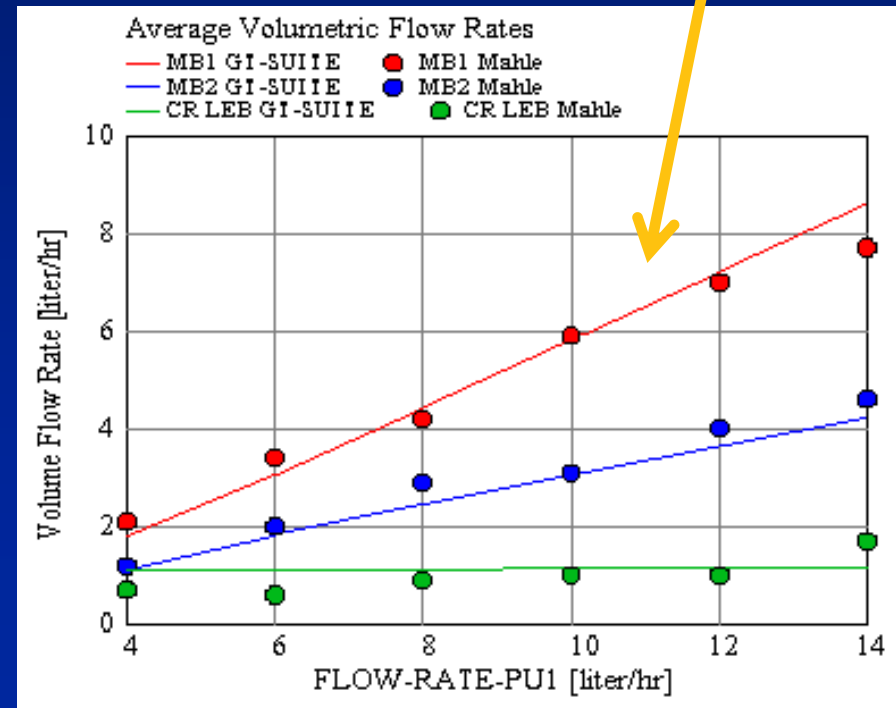
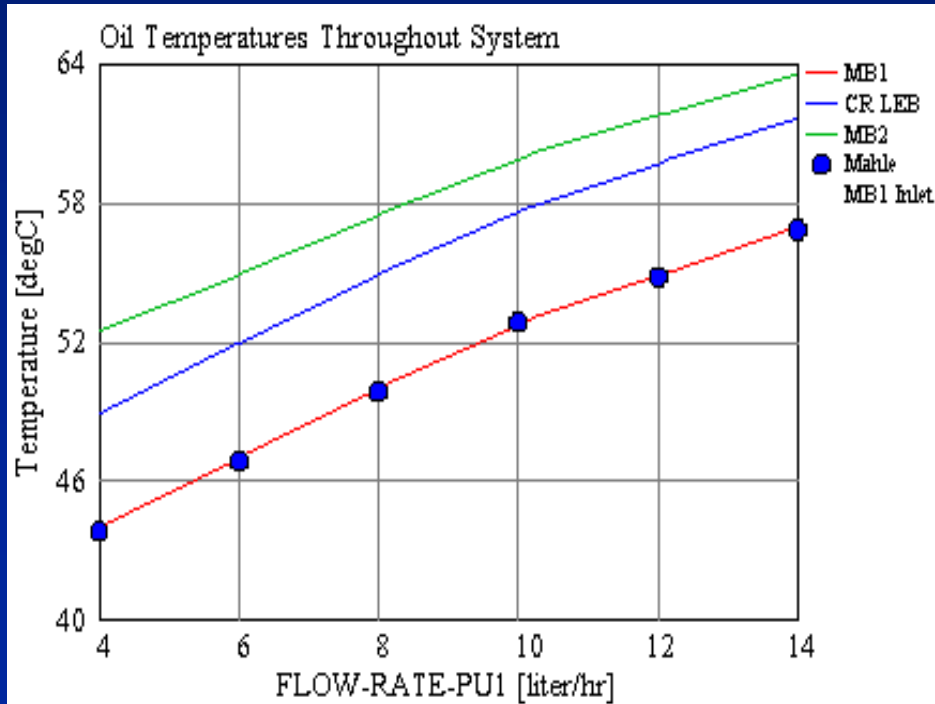




# Model Results: Step 1

- Oil temp. at MB#2 and CR LEB not known experimentally in Step 1
  - estimated in model based on bearing wall temps ( $T_{MB2} > T_{MB1}$ )
- Only tuning parameters were:
  - Temp. at MB#2 and CR LEB (see chart)
  - Restriction dia. between web drillings (0.7mm)

Flow rate distribution matches well



# Summary



## Main Findings

- **Main bearing pressure vs. flow rate through each bearing by itself correlates well to experimental data**
- **Model does not predict constant  $\Delta P$  vs.  $Q$** 
  - **Either flawed data or not modeling certain physics**

## Future Work

- **Investigate system instantaneous pressure pulsations**
- **Further validation through projects with Mahle and other customers**